



May 3, 2018

Mr. Steve Brewer, Director of Public Works
Public Works Department
Town Offices
4 Epping Street

Dear Mr. Brewer:

The Town of Raymond tasked CMA Engineers with developing preliminary design recommendations to improve the stormwater collection on Lakeview Road. This letter report summarizes the methodology and results for development of the hydrology and hydraulic analysis and the basis for our attached preliminary design.

EXISTING CONDITIONS

Although there are some grass lined swales on Lakeview Road at the top of the hill on Lakeview Road, most of the stormwater is currently collected in paved swales at the edge of the traveled way. The paved swales transport the stormwater along the roadside to the bottom of the hill either over driveways or through the occasional driveway culvert. At the bottom of the hill, there is a single catch basin that captures some of the stormwater and discharges it into Governors Lake via a culvert, but most of the flow continues overland over the beach before entering Governors Lake.

Approximately halfway down the hill, the northern drainage swale travels off the roadside and into an overland swale. The overland swale carries this stormwater, and additional runoff it picks up along the way, in a backyard grass/paved drainage swale to the bottom of the hill where it enters a road cross culvert at Water Street, discharging into a wetland, and then into Governors Lake. The drainage swale is on private property until it crosses under Water Street.

Historically, Governors Lake has had issues with Total Phosphorus (TP), chlorides, and chlorophyll. Currently, the stormwater from Lakeview Road is discharged untreated into Governors Lake. The stormwater from the culvert under Water Street is discharged to an existing wetland, which provides some treatment prior to its discharge into the lake. The Town is interested in evaluating stormwater treatment approaches to provide treatment for total suspended solids and to decrease phosphorus discharges to the lake. Lakeview Road is treated with chloride in the winter to maintain safe road conditions on the steep road. It should be noted that there are no stormwater treatment options that would reduce chloride. Due to its steep slope, reduced road salting is not recommended for Lakeview Road. Reduced road salting might be considered for some of the flatter road sections around the lake, and for relatively flat driveways.

HYDROLOGY

The hydrologic model was created using Autodesk's 'Storm and Sanitary' watershed modelling software,

and the overall watershed was split into three sub-watersheds: the upper watershed flowing into the backyard drainage swale, the backyard drainage swale watershed, and the lower watershed flowing into the beach.

The runoff curve number (CN) used in the model for each of the watersheds represents a weighted average based on the percentage of Soil Groups A, B, C, D, and open water present, as applicable. Soil maps generated by the Natural Resources Conservation Service's (NRCS) Web Soil Survey were used to determine the total area of each soil group.

The Time of Concentration (TOC) for each of the watersheds was calculated based on the summation of times for sheet flow, shallow concentrated flow, and channel flow. The flow lengths for each of the three flow types were measured from a to-scale site plan developed in Autodesk Civil 3D. The topographic information provided from the Town and prepared by Doucet Survey was overlaid on the site plan to determine beginning and ending elevations used to calculate average slopes for each flow type. Based on aerial photography, the ground cover was assumed to be "woods with light underbrush" or "woodland". Cross sectional areas for channels were approximated and then checked to ensure they were not acting as constrictions. For each of the sub-basins, multiple flow paths were checked when determining the controlling TOC. Multiple paths were evaluated to analyze different combinations of lengths, slopes, and flow types.

Below is a brief description of the watersheds and a summary table of the watersheds' properties.

The upper watershed begins at the top of the hill on Lakeview Drive and ends at the point where the runoff travels to the overland swale. This watershed accounts for all the stormwater that flows into the start of the overland drainage swale. The watershed is generally woods and larger house lots, so Woodland and 2 acre lots with Type B and Type C soils were used to determine the average curve number of the watershed.

The backyard drainage swale watershed begins at the end of the upper watershed and terminates at the drainage culvert Water St. This watershed accounts for the additional stormwater flowing into the drainage swale before it enters the culvert. The watershed is generally small house lots, so ¼ acre house lots with Type B and Type C soils were used to determine the average curve number of the watershed.

The lower watershed begins at the end of the upper watershed on the south side of the road and terminates at the Lakeview Road Beach. This watershed accounts for all the stormwater that flows into the beach. The watershed is generally small house lots, so ¼ acre house lots with Type A, Type B, and Type C soils were used to determine the average curve number of the watershed.

Table 1: Watershed Summary

Watershed	Area (ac)	Curve Number	Time of Concentration (min)
Upper Watershed	1.67	67.5	28.8
Overland Drainage Swale Watershed	0.87	79	12.7
Lower Watershed	1.96	76.5	16.5

The amount of precipitation that falls on the site, and its intensity, was determined from various sources. When performing a hydrologic analysis, standard practice in the Northeast is to use the Soil Conservation

Center’s (SCS) rainfall distribution curve, and Strafford County is in the Type III zone. To determine the amount of precipitation, Cornell University’s Northeast Regional Climate Center (NRCC), which studies and researches climate, and pertinent to this report, has published precipitation amounts for the Northeast based on historical rainfall data that are summarized in Table 2: Rainfall Summary below.

Table 2: Rainfall Summary

Storm Event	Rainfall (inches)
2	3.01
10	3.80
25	5.75
50	6.88

The analysis included the 2-, 10-, 25-, and 50- year storm events. The site was modelled for the 2- through 50-year storm events to determine peak flow rates for the different storm events. Table 3 below summarizes the hydrology results for the three watersheds. Attachment A provides information on the watershed and analysis results for the 10-year storm event.

Table 3: Hydrology Summary

Watershed	Storm Event	Stormwater Runoff (cfs)
Upper Watershed	2	0.6
	10	1.1
	25	2.7
	50	3.7
Overland Drainage Swale Watershed	2	0.9
	10	1.4
	25	2.7
	50	3.5
Lower Watershed	2	2.0
	10	2.7
	25	5.3
	50	7.0

The “first flush”, or 1-inch storm event, has the highest concentration of pollutants in stormwater runoff and is used to size stormwater treatment systems in New Hampshire. NHDES has developed, and distributes, a worksheet tool to calculate the Water Quality Volume (WQV) and Water Quality Flow (WQF) to size treatment systems. Entering the watershed data into the worksheet, the WQV and WQF for the entire watershed are 4,345 cubic feet and 0.25 cubic feet per second. See Attachment B for the WQV and WQF calculation results.

RECOMMENDATIONS

Below are preliminary recommendations with budget estimates to improve the stormwater collection system on Lakeview Road and to treat the collected stormwater before it flows into Governors Lake. The preliminary budget estimates are included for reference.

Lakeview Road Stormwater Collection Improvements

We reviewed the existing stormwater collection system on Lakeview Road, and assessed it based on its function and site limitations.

The limitations are a narrow roadway and right-of-way, proximity of homes close to the roadway, and the likelihood of shallow depth to ledge that all limit the ability to install typical structural collection devices outside of the roadway or under the roadway.

Currently, stormwater is generally collected in roadside and paved swales and transported to the bottom of Lakeview Road. The stormwater generated on the northerly side of Lakeview Road travels off the roadway and into a backyard drainage swale. This reduces the stormwater flowing alongside Lakeview Road to the bottom of the hill.

In general, continuing the existing stormwater collection system with minor changes (as noted in the attached preliminary plans and details) as the Town reconstructs Lakeview Road appears to be a reasonable project approach from an engineering and project standpoint. Installing storm drains and catch basins up to the top of the hill would be very costly, and is not merited in this circumstance, in our opinion.

In reconstructing the roadway itself, we recommend reclaiming the existing pavement, fine grading the road to reestablish a typical crown and roadway cross slope, and installation of 3 ½ inches combined of base and wearing course pavements. Additionally, reclaim material is generally too fine to meet the gradation requirements of NHDOT Item 304.3-Crushed Stone, so 1 ½ inch crushed stone is incorporated into the reclaim if needed to meet the specification requirements. Since fine grading will likely create a surplus of material, this material could be collected and reused to improve the road base materials for Water Street and the beach parking area.

Lakeview Road Beach Stormwater Treatment Alternatives

Four options were considered to treat the stormwater prior to its discharge into Governors Lake.

Catch Basin Treatment Only

The catch basin approach carries the lowest cost to the Town, but it will also have minimal effect on improving the quality of the stormwater. At a minimum, we would recommend the installation of Catch Basins #1 - #4 as shown on the preliminary plan to maximize the amount of stormwater collected, so it does not flow over the beach. Also, we would maintain the current discharge point at the bottom of Lakeview Road instead of redirecting the stormwater down Water Street. The installation of deep sump catch basins is generally considered to reduce Total Suspended Solids (TSS) by 25 percent as reported in Mass DEP's Stormwater Handbook, but it will have minimal, if any, impact on improving total phosphorus. The preliminary budget estimate to make these improvements is approximately \$71,000.

UNH's Sectional Media Filter

The UNH Stormwater Center recently developed the Sectional Media Filter (SMF) to treat stormwater in urban environments. The City of Dover has installed a few SMF's, and since it is a new technology, stormwater treatment data is not available, but UNH expects preliminary results in the upcoming year.

The SMF filter consists of two chambers: a sediment and floatable collection chamber and a treatment chamber with the two chambers separated by a weir wall and trash rack. The first chamber acts like a deep

sump catch basin and allows sediment to settle out and retain floatables. The second chamber has the media filter and provides treatment to the stormwater. The Stormwater Center reports the media filter is rated to provide treatment to 0.25 cfs of stormwater per filter media section, and based on NHDES's WQF calculator, a single filter section is required. The filter media operates on the same concept as ACF's FocalPoint system (see below), but due to the considerable size difference between the two units, we would not expect the SMF to have comparable treatment efficacy as the FocalPoint. The SMF provides a filter medium with a depth of six inches, and a surface area of 32 square feet, designed to treat the first flush of 0.25 cfs. This is 1/3 the filter medium depth and about 7% of the surface area of the FocalPoint treatment system described below to treat the same flow.

Regular maintenance of the SMF unit would consist of opening the cover over the sediment chamber and using a vacuum truck to remove the collected sediment and floatables, at a frequency to be determined by operating experience. The media filter will need to be replaced periodically, and this would require removal of the top cover, so the entire media filter can be removed with a vacuum truck and replaced with new media. Since the SMF unit is underground, and removal of the top cover is required, it should be located in an off-pavement area that can be accessed by a backhoe and vacuum truck.

Excavation below groundwater level would be required for the installation of this treatment unit. For cost purposes, we have assumed that simple trench dewatering by construction sump pumps would suffice. Borings and assessment of dewatering methods required would need to be completed in final design.

A wetlands permit would be required, at a minimum, for the installation of the outlet pipe from the treatment unit. A minor permit is anticipated.

The preliminary budget estimate, including the sectional media filter and site work, is approximately \$229,000.

ACF's FocalPoint Biofiltration System

Two aboveground solutions were investigated, and ACF Environmental's FocalPoint is the first. The FocalPoint is a proprietary system that was developed to treat, and temporarily store, stormwater in a treatment device that functions at grade and below ground. Stormwater treatment starts with deep sump catch basins to provide pretreatment and TSS removal, after which stormwater is discharged into a landscaped containment area that allows the stormwater to flow through the proprietary media filter being treated on its flow through the filter. Below the media filter is a tank system that temporarily stores the stormwater while it infiltrates into the ground. The FocalPoint has an overflow at both levels to help prevent overwhelming the treatment system. The FocalPoint has been approved for use by the NH DES Alteration of Terrain Bureau, and through independent lab testing, ACF reports 91% TSS removal, 66% TP removal, and 48% Nitrogen removal. Since the proposed upgrades include deep sump catch basins providing pretreatment for the FocalPoint system, there should be little sediment entering Governors Lake from the runoff generated by Lakeview Road. Since the discharge from the unit is below grade, and discharges near the Governors Lake water shore, the significant reduction in TSS is an important feature.

As designed, the FocalPoint would only treat stormwater generated by Lakeview Road and the overland swale would continue as it currently does, flowing through the culvert under Water Street and discharging into the wetland adjacent to the beach.

Also, of the options investigated, the FocalPoint is the only BMP that can meet the State's WQV requirements and infiltrate the WQV into the groundwater, but it is our opinion that with the proximity any of the treatment devices to Governors Lake, infiltration of the WQV has minimal benefit.

Dewatering requirements would need to be further investigated for this alternative as well.

Wetlands permitting requirements will consist of impacts to the wetlands because of site grading and installation of the discharge pipe near the shore of Governors Lake. A Minor permit is anticipated.

The FocalPoint carries the highest construction cost of the alternatives investigated. ACF estimates the unit costs approximately \$200/sf installed, and ACF has preliminarily estimated the unit will be approximately 450 square feet. The preliminary budget estimate, including the FocalPoint and site work, is approximately \$326,000.

Level Spreader with Grass Filter Strip

The second above ground solution, and our recommended stormwater treatment device, is a level spreader with a grass filter strip. This system includes the deep sump catch basins (providing TSS pretreatment) and an overland swale to collect the stormwater and discharge it into a plunge pool. The plunge pool combines the stormwater from the two sources and acts as a stilling basin to allow more TSS to settle out.

The stormwater spills over the plunge pool and flows to the level spreader which distributes the stormwater over a 35-foot-long weir, reducing the stormwater velocity, and allowing for stormwater treatment in the downstream grass filter strip. Level spreaders with grass filter strips are reported to have approximately 30% TSS removal, 20% TP removal, and 10% Nitrogen removal as reported in Pennsylvania's Stormwater BMP manual. This option also has the benefit of flowing through the existing downstream wetland/riparian buffer after it leaves the grass strip for additional treatment.

The bulk of the construction for this option will occur within an existing wooded wetland, so a wetlands permit will be required. Also, due to the extent of the wetlands disturbance it may qualify as a Major permit and/or wetlands mitigation. If the project requires a Major permit, the Army Corps of Engineers is required to review the permit application, and NH DES Wetland Mitigation Program will need to be consulted if mitigation is a project condition.

Although the level spreader with grass filter strip doesn't provide the same level of treatment as the FocalPoint, it does carry a significantly lower cost. The preliminary budget estimate for the level spreader and site work is approximately \$208,000.

A summary of the stormwater treatment alternatives is presented in Table 4 below.

Table 4 Summary of Lakeview Road Stormwater Treatment Alternatives

Alternative	Estimated Removal Efficiency		Estimated Cost
	TSS	Total P	
Current System	0%	0%	
Catch Basin Treatment	25%	N/A	\$71,000
Sectional Media Filter	25%+	UNK	\$229,000
Biofiltration System	91%	66%	\$326,000
Level Spreader/Grass Filter	30%+	20%+	\$208,000

Note that the level spreader/grass filter alternative would provide better treatment than indicated in the above table because the water from the grass filter would flow into an existing wetland for further treatment prior to being discharged to Governor's Lake. There is not a tool available for estimating that additional treatment with reasonable accuracy.

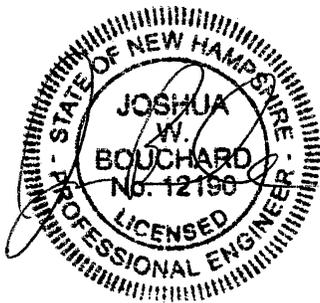
Each of these alternatives would require permitting and final design.

We have appreciated the opportunity to be of service to the Town of Raymond in this capacity. Should you have questions or comments, please don't hesitate to contact us.

Very truly yours,
CMA ENGINEERS, INC.


Joshua W. Bouchard, P.E.
Project Manager


Craig N. Musselman, P.E., BCEE
President



Attachment A

Autodesk® Storm and Sanitary Analysis 2016 - Version 12.0.42 (Build 0)

Project Description

File Name 1099-Drainage Analysis-Split.SPF

Analysis Options

Flow Units cfs
Subbasin Hydrograph Method. SCS TR-20
Time of Concentration..... SCS TR-55
Link Routing Method Hydrodynamic
Storage Node Exfiltration.. None
Starting Date MAR-07-2018 00:00:00
Ending Date MAR-08-2018 00:00:00
Report Time Step 00:05:00

Element Count

Number of rain gages 1
Number of subbasins 3
Number of nodes 4
Number of links 4

Raingage Summary

Gage ID	Data Source	Data Type	Recording Interval
Rain Gage-01	10-Yr Storm	CUMULATIVE	6.00 min

Subbasin Summary

Subbasin ID	Total Area acres
LowerRoadway	1.96
OverlandDrainageSwale	0.87
UpperRoadway	1.66

Node Summary

Node ID	Element Type	Invert Elevation ft	Maximum Elev. ft	Ponded Area ft ²	External Inflow
SpreaderOutlet	JUNCTION	281.25	284.25	0.00	
SwaleInlet	JUNCTION	327.70	330.00	100.00	
GovernorsLake	OUTFALL	274.10	277.10	0.00	
Stor-01	STORAGE	281.50	284.00	0.00	

Link Summary

Link ID	From Node	To Node	Element Type	Length ft	Slope %	Manning's Roughness
OverlandSwale	SwaleInlet	Stor-01	CHANNEL	553.0	8.3538	0.0130
WaterStCulvert	Stor-01	SpreaderOutlet	CONDUIT	30.0	0.8333	0.0150
LevelSpreader	SpreaderOutlet	GovernorsLake	WEIR			
Roadway	Stor-01	SpreaderOutlet	WEIR			

Cross Section Summary

Link Design ID Flow	Shape	Depth/ Diameter	Width	No. of Barrels	Cross Sectional Area	Full Flow Hydraulic Radius
Capacity		ft	ft		ft ²	ft
cfs						

OverlandSwale	TRAPEZOIDAL	1.50	17.00	1	14.25	0.82
413.74						
WaterStCulvert	CIRCULAR	1.50	1.50	1	1.77	0.38
8.31						

Runoff Quantity	Volume acre-ft	Depth inches
Total Precipitation	1.445	3.859
Surface Runoff	0.054	0.144
Continuity Error (%)	-0.002	

Flow Routing Continuity	Volume acre-ft	Volume Mgallons
External Inflow	0.000	0.000
External Outflow	0.532	0.173
Initial Stored Volume ...	0.000	0.000
Final Stored Volume	0.004	0.001
Continuity Error (%)	0.005	

Composite Curve Number Computations Report

Subbasin LowerRoadway

Soil/Surface Description	Area (acres)	Soil Group	CN
1/4 acre lots, 38% impervious	0.29	A	61.00
1/4 acre lots, 38% impervious	0.79	B	75.00
1/4 acre lots, 38% impervious	0.88	C	83.00
Composite Area & Weighted CN	1.96		76.50

Subbasin OverlandDrainageSwale

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Soil/Surface Description	Area (acres)	Soil Group	CN
1/4 acre lots, 38% impervious	0.44	C	83.00
1/4 acre lots, 38% impervious	0.44	B	75.00
Composite Area & Weighted CN	0.87		79.00

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Subbasin UpperRoadway

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Soil/Surface Description	Area (acres)	Soil Group	CN
Woods, Good	0.83	C	70.00
2 acre lots, 12% impervious	0.83	B	65.00
Composite Area & Weighted CN	1.66		67.50

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SCS TR-55 Time of Concentration Computations Report

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Sheet Flow Equation

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$$T_c = (0.007 * ((n * L_f)^{0.8}) / ((P^{0.5}) * (S_f^{0.4}))$$

Where:

Tc = Time of Concentration (hrs)
n = Manning's Roughness
Lf = Flow Length (ft)
P = 2 yr, 24 hr Rainfall (inches)
Sf = Slope (ft/ft)

Shallow Concentrated Flow Equation

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V = 16.1345 * (Sf^{0.5}) (unpaved surface)
V = 20.3282 * (Sf^{0.5}) (paved surface)
V = 15.0 * (Sf^{0.5}) (grassed waterway surface)
V = 10.0 * (Sf^{0.5}) (nearly bare & untilled surface)
V = 9.0 * (Sf^{0.5}) (cultivated straight rows surface)
V = 7.0 * (Sf^{0.5}) (short grass pasture surface)
V = 5.0 * (Sf^{0.5}) (woodland surface)
V = 2.5 * (Sf^{0.5}) (forest w/heavy litter surface)
Tc = (Lf / V) / (3600 sec/hr)

Where:

Tc = Time of Concentration (hrs)
Lf = Flow Length (ft)
V = Velocity (ft/sec)
Sf = Slope (ft/ft)

Channel Flow Equation

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$$V = (1.49 * (R^{2/3}) * (S_f^{0.5})) / n$$

$$R = A_q / W_p$$

$$T_c = (L_f / V) / (3600 \text{ sec/hr})$$

Where:

Tc = Time of Concentration (hrs)
Lf = Flow Length (ft)

R = Hydraulic Radius (ft)
 Aq = Flow Area (ft²)
 Wp = Wetted Perimeter (ft)
 V = Velocity (ft/sec)
 Sf = Slope (ft/ft)
 n = Manning's Roughness

 Subbasin LowerRoadway

Sheet Flow Computations

	Subarea A	Subarea B	Subarea
C			
0.00	Manning's Roughness:	0.40	0.00
0.00	Flow Length (ft):	75.00	0.00
0.00	Slope (%):	7.00	0.00
3.00	2 yr, 24 hr Rainfall (in):	3.00	3.00
0.00	Velocity (ft/sec):	0.12	0.00
0.00	Computed Flow Time (minutes):	10.67	0.00

Shallow Concentrated Flow Computations

	Subarea A	Subarea B	Subarea
C			
0.00	Flow Length (ft):	323.31	0.00
0.00	Slope (%):	7.00	0.00
Unpaved	Surface Type:	Paved	Unpaved
0.00	Velocity (ft/sec):	5.38	0.00
0.00	Computed Flow Time (minutes):	1.00	0.00

Channel Flow Computations

	Subarea A	Subarea B	Subarea
C			
0.00	Manning's Roughness:	0.12	0.00
0.00	Flow Length (ft):	201.06	0.00
0.00	Channel Slope (%):	7.00	0.00
0.00	Cross Section Area (ft ²):	0.30	0.00
0.00	Wetted Perimeter (ft):	3.10	0.00
0.00	Velocity (ft/sec):	0.69	0.00
0.00	Computed Flow Time (minutes):	4.84	0.00

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 Total TOC (minutes): 16.52
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 Subbasin OverlandDrainageSwale

Sheet Flow Computations

		Subarea A	Subarea B	Subarea
C	Manning's Roughness:	0.40	0.00	
0.00	Flow Length (ft):	75.00	0.00	
0.00	Slope (%):	7.50	0.00	
0.00	2 yr, 24 hr Rainfall (in):	3.00	3.00	
3.00	Velocity (ft/sec):	0.12	0.00	
0.00	Computed Flow Time (minutes):	10.38	0.00	
0.00				

Shallow Concentrated Flow Computations

		Subarea A	Subarea B	Subarea
C	Flow Length (ft):	470.00	0.00	
0.00	Slope (%):	8.50	0.00	
0.00	Surface Type:	Unpaved	Unpaved	
Unpaved	Velocity (ft/sec):	4.70	0.00	
0.00	Computed Flow Time (minutes):	1.67	0.00	
0.00				

Channel Flow Computations

		Subarea A	Subarea B	Subarea
C	Manning's Roughness:	0.01	0.00	
0.00	Flow Length (ft):	155.00	0.00	
0.00	Channel Slope (%):	0.50	0.00	
0.00	Cross Section Area (ft ²):	1.23	0.00	
0.00	Wetted Perimeter (ft):	3.92	0.00	
0.00	Velocity (ft/sec):	3.74	0.00	
0.00	Computed Flow Time (minutes):	0.69	0.00	
0.00				

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 Total TOC (minutes): 12.74
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 Subbasin UpperRoadway

Sheet Flow Computations

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C                               Subarea A           Subarea B           Subarea
0.00 Manning's Roughness:           0.40             0.00
0.00 Flow Length (ft):             150.00           0.00
0.00 Slope (%):                   3.00             0.00
0.00 2 yr, 24 hr Rainfall (in):    3.00             3.00
3.00 Velocity (ft/sec):            0.10             0.00
0.00 Computed Flow Time (minutes): 26.08            0.00
0.00

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Shallow Concentrated Flow Computations

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C                               Subarea A           Subarea B           Subarea
0.00 Flow Length (ft):             204.00           0.00
0.00 Slope (%):                   8.80             0.00
0.00 Surface Type:                 Woodland          Unpaved
Unpaved Velocity (ft/sec):         1.48             0.00
0.00 Computed Flow Time (minutes): 2.30             0.00
0.00

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Channel Flow Computations

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C                               Subarea A           Subarea B           Subarea
0.00 Manning's Roughness:           0.01             0.00
0.00 Flow Length (ft):             510.00           0.00
0.00 Channel Slope (%):             8.50             0.00
0.00 Cross Section Area (ft²):       1.00             0.00
0.00 Wetted Perimeter (ft):         2.00             0.00
0.00 Velocity (ft/sec):             21.05            0.00
0.00 Computed Flow Time (minutes): 0.40             0.00
0.00

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Total TOC (minutes):                28.78
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Subbasin Runoff Summary

Subbasin ID	Total Precip in	Total Runoff in	Peak Runoff cfs	Weighted Curve Number	Time of Concentration days	hh:mm:ss
LowerRoadway	3.80	1.62	2.65	76.500	0	00:16:31
OverlandDrainageSwale	3.80	1.80	1.42	79.000	0	00:12:44

UpperRoadway 3.80 1.05 1.09 67.500 0 00:28:46

Node Depth Summary

Node ID	Average Depth Attained ft	Maximum Depth Attained ft	Maximum HGL Attained ft	Time of Max Occurrence days hh:mm	Total Flooded Volume acre-in	Total Time Flooded minutes	Retention Time hh:mm:ss
SpreaderOutlet	0.02	0.14	281.39	0 12:31	0	0	0:00:00
SwaleInlet	0.01	0.08	327.78	0 12:30	0	0	0:00:00
GovernorsLake	0.00	0.00	274.10	0 00:00	0	0	0:00:00
Stor-01	0.18	1.02	282.52	0 12:30	0	0	0:00:00

Node Flow Summary

Node ID	Element Type	Maximum Lateral Inflow cfs	Peak Inflow cfs	Time of Peak Inflow Occurrence days hh:mm	Maximum Flooding Overflow cfs	Time of Peak Flooding Occurrence days hh:mm
SpreaderOutlet	JUNCTION	0.00	3.58	0 12:31	0.00	
SwaleInlet	JUNCTION	1.08	1.08	0 12:30	0.00	
GovernorsLake	OUTFALL	0.00	3.58	0 12:31	0.00	
Stor-01	STORAGE	3.99	4.61	0 12:20	0.00	

Storage Node Summary

Storage Node ID	Maximum Total Pondered Exfiltration Rate cfm	Maximum Pondered Exfiltration Volume 1000 ft ³	Maximum Pondered Exfiltrated Volume (%)	Time of Max Pondered Volume days hh:mm	Average Pondered Volume 1000 ft ³	Average Pondered Volume (%)	Maximum Storage Node Outflow cfs
Stor-01	0.00	0.103	41	0 12:30	0.018	7	3.58

Outfall Loading Summary

Outfall Node ID	Flow Frequency (%)	Average Flow cfs	Peak Inflow cfs

GovernorsLake	58.94	0.45	3.58

System	58.94	0.45	3.58

Link Flow Summary

Link ID	Ratio of Total Maximum Flow Depth	Element Reported Type Condition	Time of Peak Flow Occurrence	Maximum Velocity Attained	Length Factor	Peak Flow during Analysis	Design Flow Capacity	Ratio of Maximum /Design Flow
	Surcharged minutes		days hh:mm	ft/sec		cfs	cfs	Flow
OverlandSwale	0.37	CHANNEL Calculated	0 12:30	0.41	1.86	1.08	413.74	0.00
WaterStCulvert	0.39	CONDUIT Calculated	0 12:31	5.68	11.65	3.58	8.31	0.43
LevelSpreader	0.05	WEIR	0 12:31			3.58		
Roadway	0.00	WEIR	0 00:00			0.00		

Highest Flow Instability Indexes

All links are stable.

WARNING 107 : Initial water surface elevation defined for Junction SpreaderOutlet is below junction invert elevation.
Assumed initial water surface elevation equal to invert elevation.

WARNING 107 : Initial water surface elevation defined for Junction SwaleInlet is below junction invert elevation.
Assumed initial water surface elevation equal to invert elevation.

WARNING 110 : Initial water surface elevation defined for Storage Node Stor-01 is below storage node invert elevation.
Assumed initial water surface elevation equal to invert elevation.

WARNING 119 : Weir crest invert elevation defined for Weir LevelSpreader is below upstream node invert elevation.
Assumed weir crest invert elevation equal to upstream node invert elevation.

WARNING 117 : Conduit outlet invert elevation defined for Conduit OverlandSwale is below downstream node invert elevation.
Assumed conduit outlet invert elevation equal to downstream node invert elevation.

WARNING 002 : Max/rim elevation (depth) increased to account for connecting conduit height dimensions for Node SpreaderOutlet.

Analysis began on: Wed May 02 10:09:03 2018
Analysis ended on: Wed May 02 10:09:04 2018
Total elapsed time: 00:00:01

CMA ENGINEERS, Inc.

Civil/Environmental Engineers
 35 Bow Street
 Portsmouth, NH 03801

PROJECT NAME: **Lakeview Road**

PROJECT NO.: 1099

SHEET NO.: 1 OF 1

CALCULATED BY: SJE DATE: 5/2/2018

CHECKED BY: JWB DATE: 5/2/2018

Lakeview Road Drainage Improvements
 Catch Basin Treatment Option Estimate (Option #1)

Item #	NHDOT#	Item Description	U	Quantity	Cost	Item Cost (\$)
General Improvements						
1		Site Preparation	LS	1	\$5,000.00	\$ 5,000.00
2		4' Catch Basins	EA	2	\$3,000.00	\$ 6,000.00
3		5' Catch Basins	EA	2	\$5,000.00	\$ 10,000.00
4	603.6	15" CPP	LF	130	\$80.00	\$ 10,400.00
5		Crushed Gravel	CY	94	\$30.00	\$ 2,816.67
6	403.11	Hot Bituminous Pavement-Machine Method	TON	11	\$100.00	\$ 1,056.25
7	403.12	Hot Bituminous Pavement-Hand Method	TON	5	\$150.00	\$ 750.00
8		Ledge Removal	CY	30	\$150.00	\$ 4,500.00
8		Mobilization	LS	1	\$10,000.00	\$ 10,000.00
					Subtotal	\$ 50,522.92

Construction Contingency (10%) \$5,100

Engineering Design & Permitting (10%) \$5,100

Construction Administration/Resident Project Representative (20%) \$10,100

Subtotal \$20,300**Budget Estimate Total \$71,000**

CMA ENGINEERS, Inc.Civil/Environmental Engineers
35 Bow Street
Portsmouth, NH 03801PROJECT NAME: **Lakeview Road**

PROJECT NO.: 1099

SHEET NO.: 1 OF 1

CALCULATED BY: SJE DATE: 5/2/2018

CHECKED BY: JWB DATE: 5/2/2018

Lakeview Road Drainage Improvements
UNH Section Media Filter Estimate (Option #2)

Item #	NHDOT#	Item Description	U	Quantity	Cost	Item Cost (\$)
Drainage Improvements						
1		Site Preparation	LS	1	\$5,000.00	\$ 5,000.00
2		Embankment In-Place	CY	100	\$10.00	\$ 1,000.00
3		4' Catch Basins	EA	2	\$3,000.00	\$ 6,000.00
4		5' Catch Basins	EA	2	\$5,000.00	\$ 10,000.00
5	604.324	4' Drainage Manhole	EA	1	\$3,000.00	\$ 3,000.00
6	604.326	5' Drainage Manhole	EA	1	\$4,000.00	\$ 4,000.00
7	603.6	15" CPP	LF	326	\$80.00	\$ 26,080.00
8	209.411	Gravel	CY	235	\$30.00	\$ 7,063.33
9	403.12	Hot Bituminous Pavement-Hand Method	TON	5	\$150.00	\$ 750.00
10		Ledge Removal	CY	50	\$150.00	\$ 7,500.00
11		Mobilization	LS	1	\$5,000.00	\$ 5,000.00
Subtotal						\$ 75,393.33

Roadway Improvements-Water Street						
1		Site Preparation	LS	1	\$5,000.00	\$ 5,000.00
2		Embankment In-Place	CY	100	\$10.00	\$ 1,000.00
3		Stabilized Base Shim	CY	70	\$20.00	\$ 1,400.00
4	403.11	Hot Bituminous Pavement-Machine Method	TON	90	\$100.00	\$ 9,000.00
5		Mobilization	LS	1	\$10,000.00	\$ 10,000.00
Subtotal						\$ 26,400.00

Parking Lot Improvements						
1		Site Preparation	LS	1	\$5,000.00	\$ 5,000.00
2		Embankment In-Place	CY	100	\$10.00	\$ 1,000.00
3	606.158	Guardrail	LF	120	\$22.50	\$ 2,700.00
4		Loam & Seed	CY	42	\$45.00	\$ 1,890.00
5		Stabilized Base Shim	CY	36	\$20.00	\$ 722.96
6	403.11	Hot Bituminous Pavement-Machine Method	TON	38	\$100.00	\$ 3,830.00
7	403.12	Hot Bituminous Pavement-Hand Method	TON	7	\$150.00	\$ 984.38
8		Mobilization	LS	1	\$10,000.00	\$ 10,000.00
Subtotal						\$ 26,127.34

UNH-Sectional Media Filter						
1		Site Preparation	LS	1	\$2,500.00	\$ 2,500.00
2		Embankment In-Place	CY	100	\$10.00	\$ 1,000.00
3		Focal Point System	U	1	\$20,000.00	\$ 20,000.00
4	603.6	15" CPP	LF	50	\$80.00	\$ 4,000.00
5		Landscaping	U	1	\$2,000.00	\$ 2,000.00
6		Ledge Removal	CY	5	\$150.00	\$ 750.00
7		Mobilization	LS	1	\$5,000.00	\$ 5,000.00
Subtotal						\$ 35,250.00

Sum \$163,170.67

Construction Contingency (10%) \$16,300
Engineering Design & Permitting (10%) \$16,300
Construction Administration/Resident Project Representative (20%) \$32,600
Subtotal \$65,200

Budget Estimate Total \$229,000

CMA ENGINEERS, Inc.Civil/Environmental Engineers
35 Bow Street
Portsmouth, NH 03801PROJECT NAME: **Lakeview Road**

PROJECT NO.: 1099

SHEET NO.: 1 OF 1

CALCULATED BY: SJE DATE: 5/2/2018

CHECKED BY: JWB DATE: 5/2/2018

Lakeview Road Drainage Improvements
Focalpoint Treatment System Estimate (Option #3)

Item #	NHDOT#	Item Description	U	Quantity	Cost	Item Cost (\$)
Drainage Improvements						
1		Site Preparation	LS	1	\$5,000.00	\$ 5,000.00
2		Embankment In-Place	CY	100	\$10.00	\$ 1,000.00
3		4' Catch Basins	EA	2	\$3,000.00	\$ 6,000.00
4		5' Catch Basins	EA	2	\$5,000.00	\$ 10,000.00
5	604.324	4' Drainage Manhole	EA	1	\$3,000.00	\$ 3,000.00
6	604.326	5' Drainage Manhole	EA	1	\$4,000.00	\$ 4,000.00
7	603.6	15" CPP	LF	326	\$80.00	\$ 26,080.00
8	209.411	Gravel	CY	235	\$30.00	\$ 7,063.33
9	403.12	Hot Bituminous Pavement-Hand Method	TON	5	\$150.00	\$ 750.00
10		Ledge Removal	CY	50	\$150.00	\$ 7,500.00
11		Mobilization	LS	1	\$5,000.00	\$ 5,000.00
Subtotal						\$ 75,393.33

Roadway Improvements-Water Street						
1		Site Preparation	LS	1	\$5,000.00	\$ 5,000.00
2		Embankment In-Place	CY	100	\$10.00	\$ 1,000.00
3		Stabilized Base Shim	CY	70	\$20.00	\$ 1,400.00
4	403.11	Hot Bituminous Pavement-Machine Method	TON	90	\$100.00	\$ 9,000.00
5		Mobilization	LS	1	\$10,000.00	\$ 10,000.00
Subtotal						\$ 26,400.00

Parking Lot Improvements						
1		Site Preparation	LS	1	\$5,000.00	\$ 5,000.00
2		Embankment In-Place	CY	100	\$10.00	\$ 1,000.00
3	606.158	Guardrail	LF	120	\$22.50	\$ 2,700.00
4		Loam & Seed	CY	42	\$45.00	\$ 1,890.00
5		Stabilized Base Shim	CY	36	\$20.00	\$ 722.96
6	403.11	Hot Bituminous Pavement-Machine Method	TON	38	\$100.00	\$ 3,830.00
7	403.12	Hot Bituminous Pavement-Hand Method	TON	7	\$150.00	\$ 984.38
8		Mobilization	LS	1	\$10,000.00	\$ 10,000.00
Subtotal						\$ 26,127.34

Focalpoint Treatment System						
1		Site Preparation	LS	1	\$2,500.00	\$ 2,500.00
2		Embankment In-Place	CY	100	\$10.00	\$ 1,000.00
3		Focal Point System	SF	450	\$200.00	\$ 90,000.00
4		Landscaping	U	1	\$2,000.00	\$ 2,000.00
5	603.6	15" CPP	LF	50	\$80.00	\$ 4,000.00
6		Mobilization	LS	1	\$5,000.00	\$ 5,000.00
Subtotal						\$ 104,500.00

Sum \$232,420.67

Construction Contingency (10%) \$23,200
Engineering Design & Permitting (10%) \$23,200
Construction Administration/Resident Project Representative (20%) \$46,500
Subtotal \$92,900

Budget Estimate Total \$326,000

CMA ENGINEERS, Inc.Civil/Environmental Engineers
35 Bow Street
Portsmouth, NH 03801PROJECT NAME: **Lakeview Road**
PROJECT NO.: 1099
SHEET NO.: 1 OF 1
CALCULATED BY: SJE DATE: 5/2/2018
CHECKED BY: JWB DATE: 5/2/2018Lakeview Road Drainage Improvements
Level Spreader & Plunge Pool Estimate (Option #4)

Item #	NHDOT#	Item Description	U	Quantity	Cost	Item Cost (\$)
Drainage Improvements						
1		Site Preparation	LS	1	\$5,000.00	\$ 5,000.00
2		Embankment In-Place	CY	100	\$10.00	\$ 1,000.00
3		4' Catch Basins	EA	2	\$3,000.00	\$ 6,000.00
4		5' Catch Basins	EA	2	\$5,000.00	\$ 10,000.00
5	604.324	4' Drainage Manhole	EA	1	\$3,000.00	\$ 3,000.00
6	604.326	5' Drainage Manhole	EA	1	\$4,000.00	\$ 4,000.00
7	603.6	15" CPP	LF	326	\$80.00	\$ 26,080.00
8		Crushed Gravel	CY	235	\$30.00	\$ 7,063.33
9	403.12	Hot Bituminous Pavement-Hand Method	TON	5	\$150.00	\$ 750.00
10		Ledge Removal	CY	50	\$150.00	\$ 7,500.00
11		Mobilization	LS	1	\$5,000.00	\$ 5,000.00
Subtotal						\$ 75,393.33

Roadway Improvements-Water Street						
1		Site Preparation	LS	1	\$5,000.00	\$ 5,000.00
2		Embankment In-Place	CY	100	\$10.00	\$ 1,000.00
3		Stabilized Base Shim	CY	70	\$20.00	\$ 1,400.00
4	403.11	Hot Bituminous Pavement-Machine Method	TON	90	\$100.00	\$ 9,000.00
5		Mobilization	LS	1	\$10,000.00	\$ 10,000.00
Subtotal						\$ 26,400.00

Parking Lot Improvements						
1		Site Preparation	LS	1	\$5,000.00	\$ 5,000.00
2		Embankment In-Place	CY	100	\$10.00	\$ 1,000.00
3	606.158	Guardrail	LF	120	\$22.50	\$ 2,700.00
		Loam & Seed	CY	42	\$45.00	\$ 1,890.00
4		Stabilized Base Shim	CY	36	\$20.00	\$ 722.96
5	403.11	Hot Bituminous Pavement-Machine Method	TON	38	\$100.00	\$ 3,830.00
6	403.12	Hot Bituminous Pavement-Hand Method	TON	7	\$150.00	\$ 984.38
7		Mobilization	LS	1	\$10,000.00	\$ 10,000.00
Subtotal						\$ 26,127.34

Level Spreader & Plunge Pool						
1		Site Preparation	LS	1	\$2,500.00	\$ 2,500.00
2		Embankment In-Place	CY	100	\$10.00	\$ 1,000.00
3	203.1	Common Excavation	CY	80	\$17.00	\$ 1,360.00
4		Crushed Stone	CY	4	\$30.00	\$ 133.33
		Class C Stone	CY	8	\$50.00	\$ 388.89
		Erosion Control Fabric	SY	222	\$5.00	\$ 1,111.11
		Loam & Seed	CY	25	\$45.00	\$ 1,111.11
5	520.01	Concrete Weir	CY	3	\$900.00	\$ 2,333.33
6		Mobilization	LS	1	\$5,000.00	\$ 5,000.00
Subtotal						\$ 14,937.78

Sum \$142,858.45

Construction Contingency (10%) \$14,300
Engineering Design & Permitting (15%) \$21,400
Construction Administration/Resident Project Representative (20%) \$28,600
Subtotal \$64,300

Budget Estimate Total \$208,000

Town Of Raymond, New Hampshire Lakeview Road Drainage Improvements

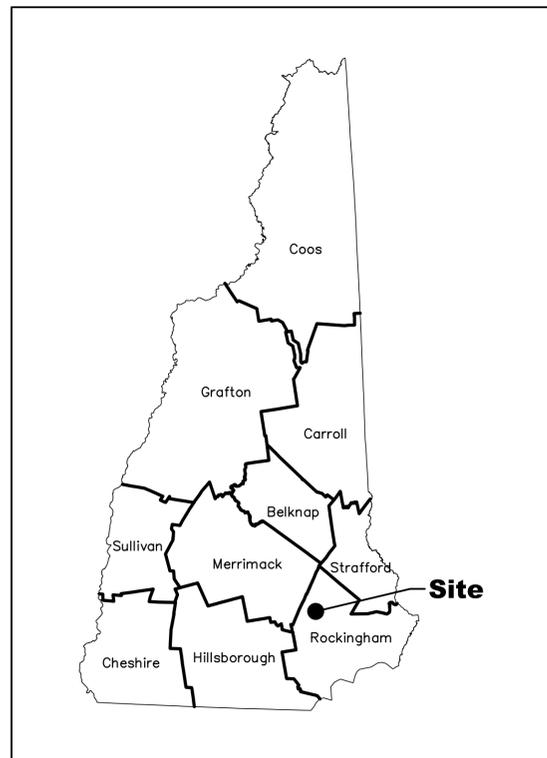
Preliminary Design May 2018

Sheet List Table		
Subset	Sheet Number	Sheet Title
--	--	Cover
EX		
	1	Existing Conditions Plan
G		
	1	General Plan (1)
	2	General Plan (2)
	3	General Plan (3)
D		
	1	Miscellaneous Details



SITE OVERVIEW

SCALE: 1" = 100'



Locus Plan

Prepared For:
Town of Raymond
4 Epping Street
Raymond, NH 03077

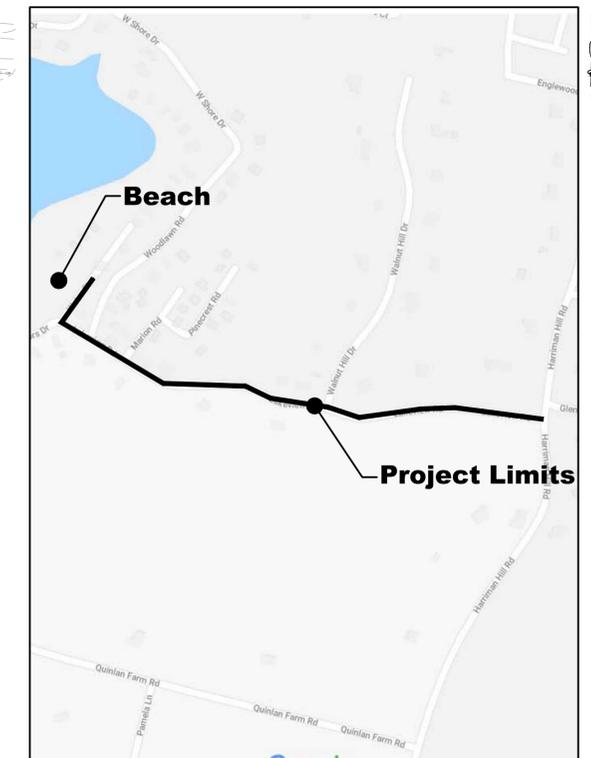
Prepared By:

CMA
ENGINEERS

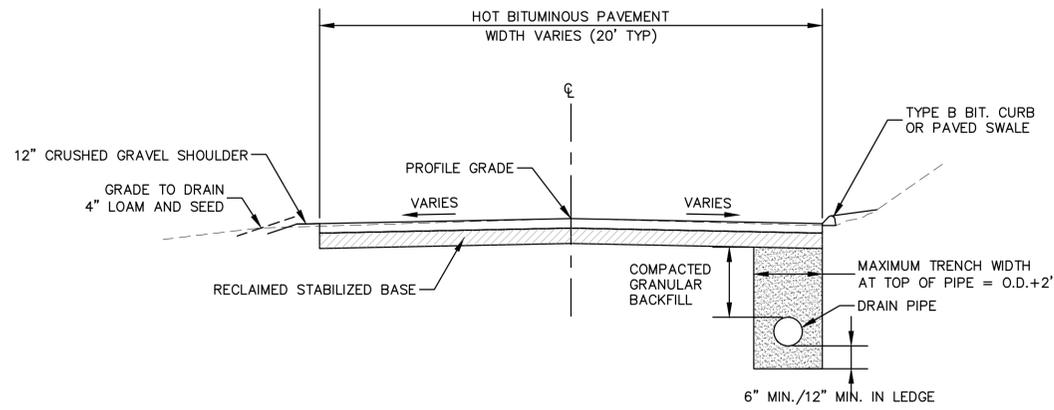
CIVIL/ENVIRONMENTAL/STRUCTURAL

Portsmouth, NH • Manchester, NH • Portland, ME
 603/431-6196 • 603/627-0708 • 207/541-4223
 cmaengineers.com

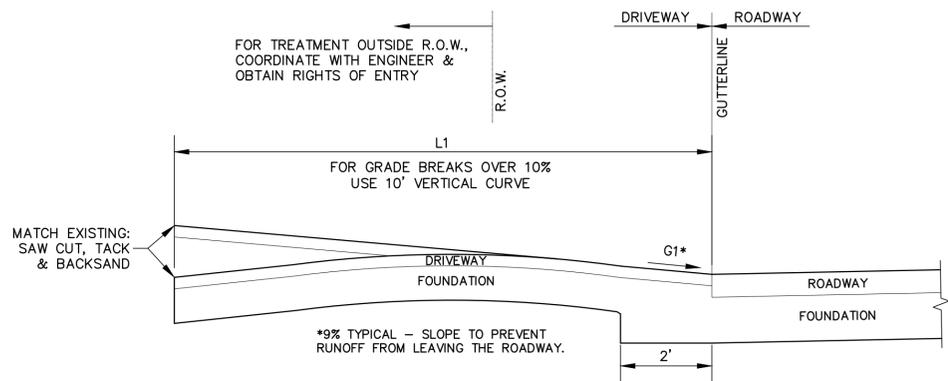
Not for Construction



Project Location

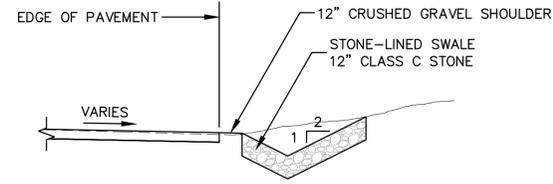


TYPICAL ROAD SECTION
NOT TO SCALE

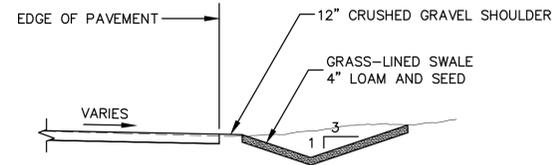


DRIVEWAY DETAIL
NOT TO SCALE

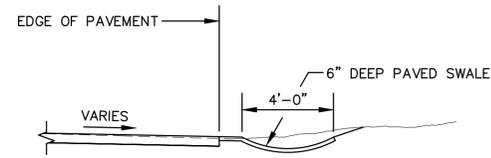
- NOTES:**
- IF THE ALGEBRAIC DIFFERENCE BETWEEN TWO ADJACENT GRADES EXCEEDS 10%, PROVIDE A 10' VERTICAL CURVE TRANSITION.
 - CURBING CAN BE FLARED TO FIT DRIVE RADII IF APPROPRIATE OR ENDED AS DETAILED ABOVE.
 - FOR UNPAVED DRIVES, THE PAVED APRON NORMALLY ENDS AT THE RADIUS TANGENT POINT.



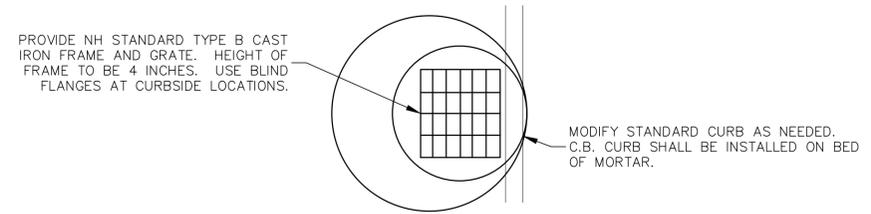
ROADSIDE STONE-LINED SWALE DETAIL
NOT TO SCALE



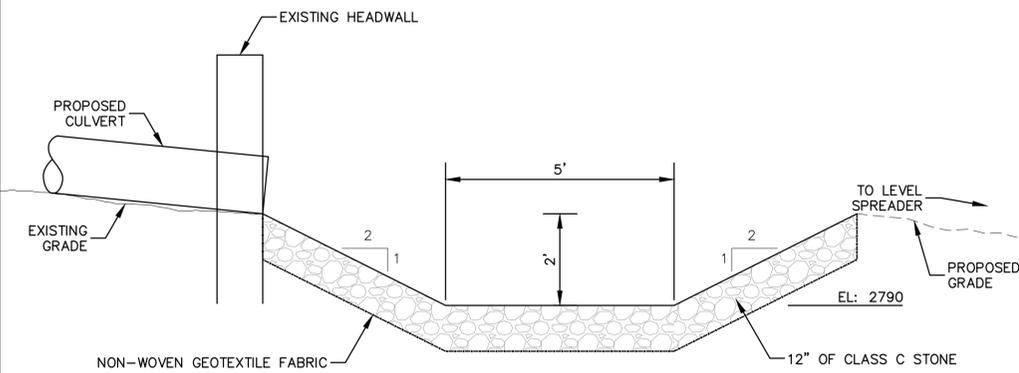
ROADSIDE GRASS-LINED SWALE DETAIL
NOT TO SCALE



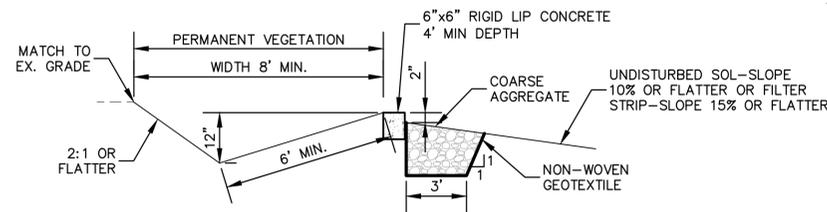
ROADSIDE PAVED SWALE DETAIL
NOT TO SCALE



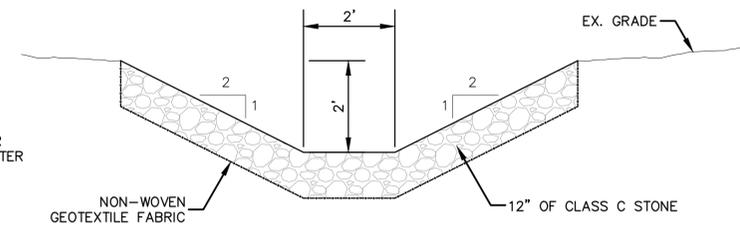
DEEP SUMP CATCH BASIN DETAIL
NOT TO SCALE



PLUNGE POOL DETAIL
NOT TO SCALE



LEVEL SPREADER DETAIL
NOT TO SCALE



STONE-LINED SWALE DETAIL
NOT TO SCALE

Not for Construction

date	May 2018	project no.	1089	file name:	1089-details.dwg	designed by:	JWB	drawn by:	JWB/SJE	approved by:	CMM	scale:	0 20' 40'	Scale: 1" = 20'
no.														
revision														
date														
no.														
<p>CMA ENGINEERS Civil/Environmental/Structural Portland, NH • 603/627-0708 • 207/641-4223 Manchester, NH • 603/431-6196</p>														
<p>PRELIMINARY DESIGN</p>														
<p>Town of Raymond, New Hampshire Department of Public Works Lakeview Road Drainage Improvements Miscellaneous Details</p>														
<p>drawing no. D-1</p>														
<p>sheet: 6 of 6</p>														